## What is claimed is:

1. An optical fiber wherein

a zero dispersion wavelength falls within a range of between 1,250 nm and 1,350 nm inclusive,

a transmission loss at 1,550 nm is equal to or less than 0.185 dB/km.

a chromatic dispersion at 1,550 nm is within a range of  $19 \pm 1$  ps/nm·km,

a dispersion slope at 1,550 nm is equal to or less than 0.06 ps/nm<sup>2</sup>·km,

an effective area  $A_{\rm eff}$  at 1,550 nm is equal to or more than 105  $\mu m^2$ , a cable cutoff wavelength  $\lambda_{cc}$  is equal to or less than 1,530 nm, polarization mode dispersion at 1,550nm is equal to or less than 0.1

ps/km<sup>1/2</sup>, and

a macrobending loss at 1,550 nm when the optical fiber is wound on a mandrel having an outer diameter of 20 mm is equal to or less than 10 dB/m.

2. An optical fiber comprising:

a first region provided in a center of the optical fiber, having a refractive index difference  $\Delta n1$  relative to a refractive index n0 of silica and an outer diameter of a;

a second region formed around said first region, having a refractive index difference  $\Delta n2$  relative to the refractive index n0 of silica and an outer diameter of b;

a third region formed around said second region, having a refractive index difference  $\Delta n3$  relative to the refractive index n0 of silica and an outer diameter of c;

a fourth region formed around said third region, having a refractive index difference  $\Delta n4$  relative to the refractive index n0 of silica and an outer diameter of d; and

a fifth region formed around said fourth region, having a refractive index difference  $\Delta n5$  relative to the refractive index n0 of silica and an outer diameter of e,

in which the refractive index differences  $\Delta n1$  through  $\Delta n5$  satisfy a relationship as follows:

 $\Delta n2 < \Delta n4 < \Delta n3 < \Delta n1$   $\Delta n1$ ,  $\Delta n2$ ,  $\Delta n3$ ,  $\Delta n4 < 0$  $\Delta n5 > 0$ 

3. The optical fiber as claimed in claim 2, wherein the outer diameter a of said first region, the outer diameter b of said second region and the outer diameter c of said third region satisfy a relationship as follows:

 $1.20 \le b/a \le 2.00$ 

 $1.44 \le c/a \le 4.00$ .

4. The optical fiber as claimed in claim 2, wherein the refractive index differences  $\Delta n1$ ,  $\Delta n2$  and  $\Delta n3$  are defined as follows:

 $-0.1\% < \Delta n1 < 0\%$ 

 $-0.5\% \le \Delta n2 \le -0.2\%$ 

 $-0.4\% \le \Delta n3 \le -0.1\%$ .

5. The optical fiber as claimed in claim 2, wherein the outer diameter e of said fifth region and the outer diameter d of said fourth region satisfy a relationship as follows:

 $0.040 \le {(e-d)/2}/e \le 0.096.$ 

6. The optical fiber as claimed in claim 2, wherein the outer diameter e of said fifth region and the outer diameter d of said fourth region satisfy a relationship as follows:

 $e=125\ \mu m$ 

 $5 \ \mu \text{m} \le \{(\text{e-d})/2\} \le 12 \ \mu \text{m}.$ 

7. An optical fiber comprising:

a first region provided in a center of the optical fiber, having a germanium concentration of  $C_{Gel}$  (mol%) and a fluorine concentration of  $C_{Fl}$  (mol%);

a second region formed around said first region, having a germanium concentration of  $C_{Ge2}$  (mol%) and a fluorine concentration of  $C_{F2}$  (mol%);

a third region formed around said second region, having a germanium concentration of  $C_{Ge3}$  (mol%) and a fluorine concentration of  $C_{F3}$  (mol%);

a fourth region formed around said third region, having a germanium concentration of  $C_{Ge4}$  (mol%) and a fluorine concentration of  $C_{F4}$  (mol%); and

a cladding portion formed around said fourth region,

in which the germanium concentrations  $C_{Ge1}$  through  $C_{Ge4}$  and fluorine concentrations  $C_{F1}$  through  $C_{F4}$  satisfy a relationship as follows:

$$-0.1 < 0.096 \times C_{Ge1} - 0.398 \times C_{F1} < 0$$

$$-0.5 \le 0.096 \times C_{Ge2} - 0.398 \times C_{F2} \le -0.2$$

$$-0.4 \le 0.096 \times C_{Ge3} - 0.398 \times C_{F3} \le -0.1$$

$$-0.5 < 0.096 \times C_{Ge4} - 0.398 \times C_{F4} < -0.1$$

8. The optical fiber as claimed in claim 7, wherein the germanium concentrations  $C_{Ge1}$  through  $C_{Ge4}$  and fluorine concentrations  $C_{F1}$  through  $C_{F4}$  satisfy a relationship as follows:

$$C_{Ge1}$$
,  $C_{Ge2}$ ,  $C_{Ge3}$ ,  $C_{Ge4} = 0$   
 $C_{F1}$ ,  $C_{F2}$ ,  $C_{F3}$ ,  $C_{F4} > 0$ .

9. The optical fiber as claimed in claim 7, wherein the germanium concentrations  $C_{Ge1}$  through  $C_{Ge4}$  and fluorine concentrations  $C_{F1}$  through  $C_{F4}$  satisfy a relationship as follows:

$$\begin{split} &C_{Ge1},\,C_{F1}>0\\ &C_{Ge2},\,C_{Ge3},\,C_{Ge4}=0\\ &C_{F2},\,C_{F3},\,C_{F4}>0. \end{split}$$

10. The optical fiber as claimed in claim 7, wherein

the germanium concentrations  $C_{Ge1}$  through  $C_{Ge4}$  and fluorine concentrations  $C_{F1}$  through  $C_{F4}$  satisfy a relationship as follows:

$$\begin{split} &C_{Ge1},\,C_{F1}>0\\ &C_{Ge2}=0,\,C_{F2}>0\\ &C_{Ge3},\,C_{F3}>0\\ &C_{Ge4}=0,\,C_{F4}>0 \end{split}$$

11. A method for manufacturing an optical fiber which includes:

a first region provided in a center of the optical fiber, having a refractive index difference  $\Delta n1$  relative to a refractive index n0 of silica and an outer diameter of a;

a second region formed around said first region, having a refractive index difference  $\Delta n2$  relative to the refractive index n0 of silica and an outer diameter of b;

a third region formed around said second region, having a refractive index difference  $\Delta n3$  relative to the refractive index n0 of silica and an outer diameter of c;

a fourth region formed around said third region, having a refractive index difference  $\Delta n4$  relative to the refractive index n0 of silica and an outer diameter of d; and

a fifth region formed around said fourth region, having a refractive index difference  $\Delta n5$  relative to the refractive index n0 of silica and an outer diameter of e,

in which the refractive index differences  $\Delta n1$  through  $\Delta n5$  satisfy a relationship as follows:

 $\Delta n2 < \Delta n4 < \Delta n3 < \Delta n1$   $\Delta n1$ ,  $\Delta n2$ ,  $\Delta n3$ ,  $\Delta n4 < 0$  $\Delta n5 > 0$ ,

a zero dispersion wavelength of the optical fiber falls within a range of between 1,250 nm and 1,350 nm inclusive,

the first region has a germanium concentration of  $C_{Ge1}$  (mol%) and a fluorine concentration of  $C_{F1}$  (mol%),

the second region has a germanium concentration of  $C_{Ge2}$  (mol%) and a fluorine concentration of  $C_{F2}$  (mol%),

the third region has a germanium concentration of C<sub>Ge3</sub> (mol%) and

a fluorine concentration of C<sub>P3</sub> (mol%),

the fourth region has a germanium concentration of C<sub>Ge4</sub> (mol%) and a fluorine concentration of C<sub>F4</sub> (mol%), and

the germanium concentrations  $C_{Ge1}$  through  $C_{Ge4}$  and the fluorine concentrations  $C_{F1}$  through  $C_{F4}$  satisfy a relationship as follows:

$$-0.1 < 0.096 \times C_{Ge1} - 0.398 \times C_{F1} < 0$$

$$-0.5 \le 0.096 \times C_{Ge2} - 0.398 \times C_{f2} \le -0.2$$

$$-0.4 \le 0.096 \times C_{Ge3} - 0.398 \times C_{F3} \le -0.1$$

$$-0.5 < 0.096 \times C_{Ge4} - 0.398 \times C_{F4} < -0.1$$

said method wherein, in synthesizing soots which are to be said first through fourth regions, respective soot synthetic raw materials including silica are doped with predetermined amounts of germanium and/or fluorine to synthesize the soots, and

in vitrification of the soots to form a transparent glass, the soots are sintered in an atmosphere including fluorine and/or chlorine.

- 12. The method as claimed in claim 11, comprising:
- a first step of synthesizing a first soot, which is to be the first region, and heating and vitrifying the first soot to form a first glass;
- a second step of synthesizing a second soot, which is to be the second region, around the first glass formed at said first step and heating and vitrifying an obtained first glass-soot composite to form a first composite glass;
- a third step of synthesizing a third soot, which is to be the third region, around the first composite glass formed at said second step and heating and vitrifying an obtained second glass-soot composite to form a second composite glass;
- a fourth step of synthesizing a fourth soot, which is to be the fourth region, around the second composite glass formed at said third step and heating and vitrifying an obtained third glass-soot composite to form a third composite glass;
- a fifth step of synthesizing a fifth soot, which is to be the fifth region, around the third composite glass formed at said fourth step and heating and vitrifying an obtained fourth glass-soot composite to form a

fourth composite glass, which is then formed into an optical fiber preform; and

a sixth step of heating and drawing an end of the optical fiber preform to form the optical fiber.

13. An optical fiber wherein

an absolute value of a dispersion value at 1,550 nm falls with a range of between 4 ps/nm·km and 20 ps/nm·km inclusive,

a dispersion slope at 1,550 nm falls with a range of between 0.05 ps/nm<sup>2</sup>·km and 0.08 ps/nm<sup>2</sup>·km inclusive,

transmission loss at 1,550 nm is equal to or less than 0.2 dB/km, and

an effective area  $A_{\rm eff}$  at 1,550 nm is equal to or more than 80  $\mu m^2$ .

14. An optical fiber comprising:

- a center core provided in a center of the optical fiber, having a refractive index difference  $\Delta 1$  relative to a refractive index n0 of silica and an outer diameter of A;
- a side core formed around said center core, having a refractive index difference  $\Delta 2$  relative to the refractive index n0 of silica and an outer diameter of B;
- a first cladding formed around said side core, having a refractive index difference A3 relative to the refractive index n0 of silica; and

a second cladding formed around said first cladding, and

in which the refractive index differences  $\Delta 1$  through  $\Delta 3$  satisfy a relationship as follows:  $\Delta 1 > \Delta 2 > \Delta 3$ 

15. The optical fiber as claimed in claim 14, wherein the refractive index differences  $\Delta n1$ ,  $\Delta n2$  and  $\Delta n3$  are defined as follows:

 $-0.20\% \le \Delta 1 \le 0.20\%$ 

 $-0.45\% \le \Delta 2 \le -0.05\%$ 

 $-0.50\% \le \Delta 3 \le -0.20\%$ .

16. The optical fiber as claimed in claim 14, wherein the outer diameter A of said center core and the outer diameter B of said side core satisfy a relationship as follows:

## $0.3 \leq A/B \leq 0.8$ , and

a viscosity of said second cladding is higher than a viscosity of said center core.

- 17. An optical transmission channel of which an optical fiber as claimed in claim 1 or 2 is used in at least one part.
- 18. An optical transmission channel of which an optical fiber as claimed in claim 13 or 14 is used in at least one part.